PERFORMANCE TESTING PROCEDURE- May 6, 2002, AN

Test Objective- Conduct a 950 MW gross test run over an extended 3 day test period at normal operating conditions to document problems and concerns in maintaining main steam superheat and reheat temperatures including use of main steam and reheat desuperheating sprays, reheat and primary superheat bias dampers, and sootblowing Information derived from this test will help determine if additional superheat surface area is required in the boiler.

OPERATING PARAMETERS:

Future Rated Capacity- 950 MWgross **IGS UNIT 2**

Test Date and Time: 3 day test run from Tuesday 5/14/2002 17:00 to Friday 5/17/2002 15:00 (immediately following the 10 hour turbine test at Valves Wide Open/ 985 MW gross)

Load, gross	**950 MWgross**
Throttle pressure	~2350 psig
Control valve position	~50%

Normal Operating Conditions
Turbine Setup- local control, AGC- out of service
Boiler Setup- set to control desired throttle pressure. For this test series, the main objective is to achieve Main Steam and Hot Reheat temps, Econ Gas Outlet Temp (EGOT) is secondary and will be documented to determine impact on boiler efficiency.

Throttle Temperature 1005 F
During the previous high load tests, there was a calibration problem on the main steam sprays controller. Main steam spray flow was false which was helping to suppress temperatures. This problem has been resolved.

Hot Reheat Temperature 1005 F
Set up boiler to control reheat temps with gas biasing dampers (no reheat sprays, if possible). Please document if any problems.

Sootblowing
Please follow normal sootblowing schedules. However if these are inadequate please document on the Operation's- Observations Log (a copy attached to the back of this procedure).

Water and Steam Cycle Isolation- normal operational setup

Generator Power Factor- MVAR target of 50 -60, need to supply own MVAR support for Unit 2 auxiliary power. Power Factor needs to be 0.985 lagging to 1.0 (by using the other generator to supply the reactive power required by the station)

Generator Hydrogen Pressure- 63 psi or higher

Generator Transformer Bushing Monitoring System- the new generator transformer bushing monitoring system and its alarms has prevented us from conducting additional testing due to concerns with one of the bushings. However, the monitoring system itself has been identified as having a problem and we are waiting on several components to replace.

NOTES ON EQUIPMENT:

AIR COMPRESSORS- Please have **Air Compressor D** running (prior to the test), due to low bus voltage concerns. Do not start during the test series, the air compressor motors are 'small' motors with a 90% voltage start limit on them.

PULVERIZERS- 7 mill operation requested
Remove pulverizer primary air flow or coal flow bias, unless absolutely necessary
At the higher loads, losing a second pulv will probably cause a temporary unit derate (unless you have 6 really good mills)

PRIMARY AIR FANS- request PA Fans in low speed operation with PA Duct pressure of 42"wc.. During the first test, we were running out of PA damper position on the pulverizers however PA Duct pressure was 47"wc, due to 6 pulverizer operation.

BOILER CYCLE LIMITATIONS: The maximum steam flow relieving of the boiler relief valve system is **6,900 KPPH.** This is our upper capacity limitation.

BOILER FEED PUMPS: note- BFP 1B has been upgraded, so BFP 1A runs with a higher bias to keep both feed pumps with the same pressure output

BACKPRESSURE- All cooling tower fans need to be in service to achieve best condenser backpressure.. Due to cool Spring weather conditions, the cooling tower and condenser should be able to handle the heat rejection.

CLOSED CYCLE COOLING WATER TEMPERATURES- There is a concern with increased CCCW temperatures and restrictions caused by the increase in outlet circulating water temperatures. Equipment which needs to be evaluated includes the station air compressors, vacuum pumps (seal water), booster air compressors and turbine lube oil.

BURNERS/ Nox- Monitor NOx conditions and try to hold NOx levels to the 0.40 #/Mbtu by increasing out of service cooling air and lowering combustion air flow levels (O2 levels).

BAGHOUSE OPERATION- Concern with high baghouse differential pressures (will be re-scaled), but this has been addressed with the sonic horn installation. Increased gas flows and removal rates associated with higher operating loads shouldn't pose additional problems or concerns

Monitor ID fan suction pressure over-ride level (which will be re-scaled).

Scrubber Operation- Increased gas flows and removal rates associated with higher operating loads shouldn't pose additional problems or concerns with the scrubber module operation. However, monitor scrubber removal rates closely.

ELECTRICAL SYSTEM

While testing the unit at high power output (> 900 MWg) you should be aware of the following limits or constraints of the electrical system.

GENERATOR- The generator is designed for the following rated conditions:

991	MVA	26	kV	22,006	I_A
0.90	PF	5363	I_F	63	psig H_2

At loads above 891 MWg the power factor must be raised above 0.90 to stay within the generator capability curve. For testing at 975 MWg the power factor must be above 0.985 lagging. Ideally, the power factor should be set to unity by using the IGS Unit 1 generator (raising voltage and MVARS) to supply the reactive power required by the station.

In the operating range of 891 to 991 MWg the capacity of the generator is limited by armature heating. All of the generator RTDs and thermocouples should be monitored during the test to verify the temperature of the generator winding stays within design limits. Although you should monitor all of the generator temperature indications , pay particular attention to the following design and alarm limits.

Estimated water outlet temp. (46 C inlet water) at max capability	62 C
High inlet water temperature alarm	48 C (± 1 C)
High water outlet temperature alarm	81 C (± 1 C)
High water outlet temperature trip	86 C (+0/-2 C)
High stator bar outlet temp alarm	86 C (± 1 C)
High stator temp between stator bars	81 C (± 1 C)
High P bar outlet temp	65 C (± 1 C)
Estimated connection ring outlet temp at max capability	55 C
Connection ring outlet temperature alarm	65 C

The temperatures should be monitored using the TGSI system not the PI system.

The generator rating, of 991 MVA, requires a hydrogen gas pressure of 63 psig. For every 1 psi drop in hydrogen gas pressure the generator capability is reduced by 8 MW. At 61 psig, hydrogen gas pressure, the generator must be operated at unity power factor to stay within the generator capability curve, if the generator output is 975 MWg.

Generators are designed to operate continuously at rated kVA, frequency and power factor over a range of 95 to 105% of rated voltage. Operation beyond rated kVA may result in harmful stator over current. Note, at rated kVA, 95% rated voltage, stator current will be 105% . This is permissible. You should carefully monitor the stator current. Do not exceed the rated current of 22,006 amperes unless you calculate the current limit at lower operating voltages (within the ±5% of rated voltage) and you are within those limits. Do not exceed a hard limit of 23,106 amperes (if limit is approached, decrease unit load).

Do not operate above the rated kVA of the generator and try to rely on temperature indication to indicate excessive stator currents since unmonitored phenomena such as temperature in other parts of the stator circuit, winding forces, abnormal magnetic field, etc may become excessive.

Operation of the generator with lagging power factor, beyond the limits of the capability curve, may result in overheating the field winding. Increasing the field current will lower the power factor. If you try to lower the power factor (and increase the field current) beyond rated, the maximum excitation limit will activate. The maximum excitation limit is set to 105 % of rated field current (5630 amperes). If this limit is exceeded, an inverse time versus current signal is generated (the higher the current level the shorter the time). After a time delay, the generator will transfer from AC to DC control. If the field current is not reduced below 105%, by the transfer, the generator will trip.

The generator is also protected from under excitation by the underexcited reactive ampere limit. If the AC control system causes operation of the generator to be outside the capability curve (leading power factor region) the URAL control will take over and limit the excitation system. This curve is presently set to not allow leading power factor operation at 975 MWg.

ISOPHASE BUS DUCT- The isophase bus is rated for 23,100 amperes at 26 kV. At rated current, the maximum rise, above a 40 C ambient, was designed to be 65 C on the conductor and 40 C on the enclosure. Because our operating experience indicated the bus conductor and enclosure were operating at a higher temperature than design, a forced cooling system was installed on the Unit 2 Isophase Bus in March 2002. Although this cooling system only provides cooling from the generator terminal to the generator circuit breaker the rating for this section of bus is now 24,500 amperes with a 75 C rise on the conductor. The bus is presently configured to handle the maximum output of the generator (23,106 amperes) without any problems as long as the forced cooling system is running.

GENERATOR STEP-UP TRANSFORMER- The generator step-up transformer is rated at 865 MVA with a 55 C rise and 968.8 MVA with a 65 C rise. Because part of the output of the generator is sent to the auxiliary transformers the generator step-up transformer is not expected to be loaded above nameplate limits. In addition oil filled transformers have an inherent overload capability. The generator step-up transformer temperatures should be monitored during the test. The oil temperature is set to alarm at 91 C and the winding temperatures alarm at 120 C.